Maximizing the Use of Local Aggregates in Asphalt Surfaces

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Outline

- Background and Objectives
- Approach
- Findings
- Implementation

Background

- Local materials predominantly carbonates
- Limestones are susceptible to polishing
- Available high friction aggregates are steel and blast furnace slags and sandstone
 - Limited sources
 - Long haul distances
 - Premium prices
- Current limits based on historical performance

Objective

- Objective explore opportunities to allow the use of more local materials in HMA in place of "imported" fine and coarse aggregates
- Aligned with INDOT goal of reducing construction costs while maintaining level of performance.

How much local aggregate can replace high quality friction aggregate in HMA surfaces?

Experimental Approach

- Build on testing procedure developed in earlier study
- Fabricate, polish and test slabs of various compositions
 - Local coarse aggregate up to 40% blended with steel slag, ACBF and sandstone
 - Local fine aggregate up to 20%
 - Both local fine and coarse at 20%
 - 9.5 mm DGA and SMA mixes

Goals for Required Lab Method

- Test friction and texture
- Accelerate polishing
- Test asphalt mixtures, not aggregates only
- Ideal to be able to test in lab and field
- Led to identification of Dynamic Friction Tester and Circular Track Meter
- Needed a polisher to match
- Idea from NCAT, refined by NCSC

Dynamic Friction Tester (DFT)



DFT – dynamic friction at 20 km/h (DF20)

Circular Track Meter (CTM)



CTM – Mean Profile Depth, mm

International Friction Index

 $F60 = 0.081 + 0.732 DF_{20}e^{-Sp}$ $S_p = 14.2 + 89.7 MPD$

IFI (*F60*, S_p)





-40



Circular Track Polishing Machine





Texture and Friction (DF20)







Polishing Model

Initial Pavement Life Zone

Decreasing Friction Zone

Friction Stabilization Zone



Aggregates Selected for Testing

- Polish Resistant
 - Steel slag
 - Blast furnace slag
 - Sandstone
- Polish Susceptible (St. Genevieve formation)
 - 3 sources
- Polish Resistant Aggregate Carbonate (PRA)
 - 1 source

Coarse Agg in DGA – F60

Resistant/Susceptible	0%	10%	20%	40%
Steel Slag/PSI	0.33	0.29	0.28	0.23
Steel Slag/ PSII	0.33	-	0.31	-
Sandstone/PSI	0.30	_	0.27	-
ACBF/PSI	0.34		0.26	-

All at 165,000 wheelpasses.

40% is too high.

Coarse Agg in DGA with Steel Slag



Coarse Agg in SMA – F60

Resistant/Susceptible	0%	10%	20%	40%
Steel Slag/PSI	0.43	0.37	0.37	
Steel Slag/PSII	0.43	0.37	0.36	0.33
Sandstone/PSII	0.42		0.34	
ACBF/PSII	0.41	0.29	0.32	

All at 165,000 wheelpasses.

Coarse Agg in SMA with Steel Slag



Findings

- Adding polish susceptible agg caused decrease in surface friction in DGA and SMA.
- Friction was still acceptable at up to ~20% local agg.
- Fine aggregate data was somewhat erratic.
- Fine agg up to 20% had small negative effect.
- There are other considerations besides friction (shape, strength, gradation).

Other Testing

- SR62 test strip, June 2010
- Coarse Aggregates
 - Steel Slag alone
 - PRA alone
 - PRA and steel slag blend
- Samples of three mixes and aggregates provided
- Slabs prepared, compacted and tested

Mixes from Field Trial



Ultimate Product

- Laboratory screening test method for qualifying aggregates
- Set baseline for steel slag, ACBF slag, sandstone
- Aggregate producers can choose to have aggregates screened
- If they pass, go to field test
- Comparison is made to known aggregate, not a particular F60 value (at this time)
- Implemented as screening test for ESALs ≥10,000,000 (ITM 221)

Potential Cost Savings

Substituting local agg for steel slag could save:

- \$1.50 to 2 per ton of hot mix (fine aggregate)
- \$3 to 4 per ton of hot mix (coarse agg)
- \$4.50 to 6 per ton of hot mix (both)
- Up to 10% of cost of mix
- \$3000 to 4000 per lane mile of surface mix

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